

ECAL for GEp5

B. Wojtsekhowski

Electron Calorimeter For GEp5

Performance Requirements

- Function: Detect 4 to 5 GeV Electrons
- Energy resolution: $\sigma/E \sim 10\%$ for 3.5 GeV electrons
- Spatial resolution: 6-8 mm
(2 mm with upstream coordinate detector)
- Full luminosity: $8 \cdot 10^{38}$ Hz/cm²
- Trigger: 20 cm thick AL reduces background
Signal summing capabilities
Trigger at 75% of elastic peak

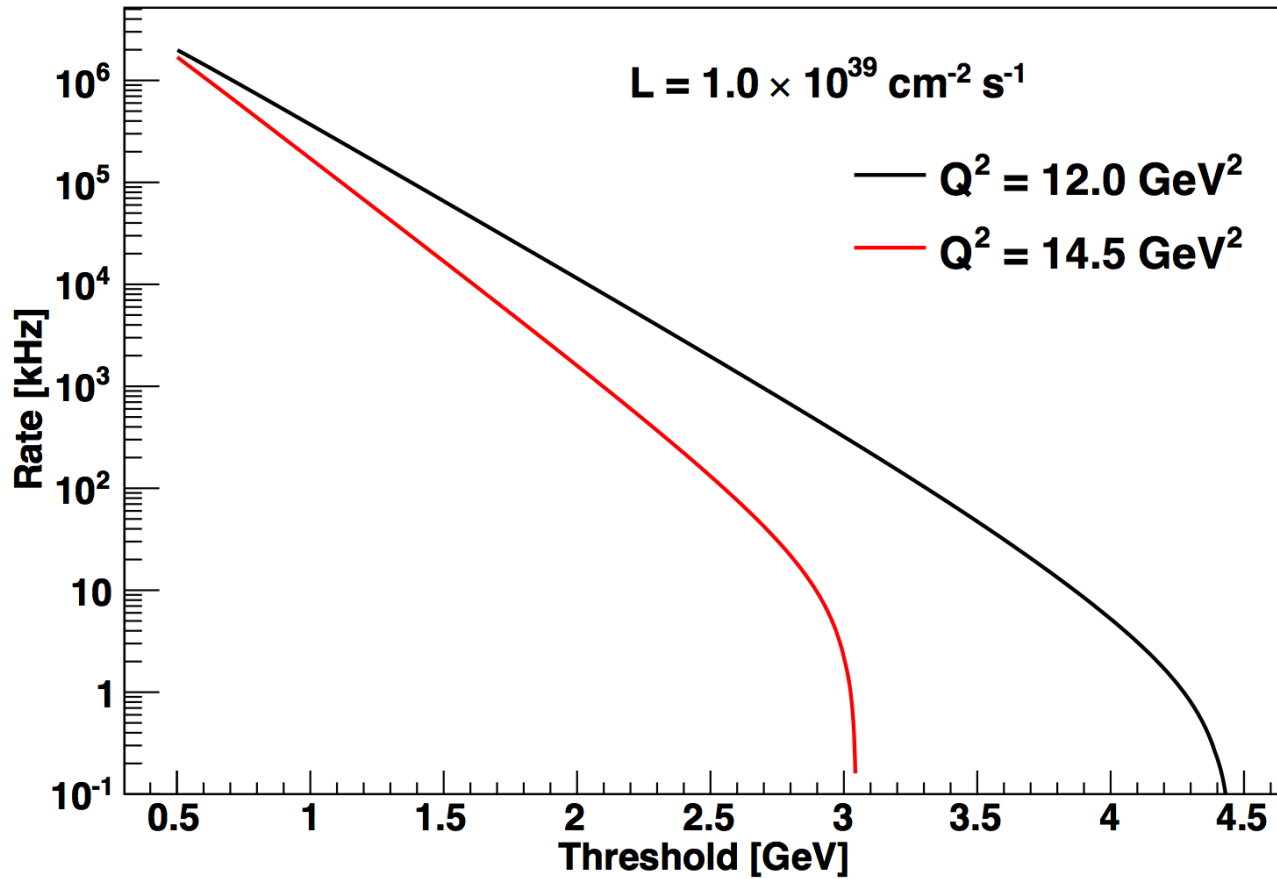
Several slides are from G.Franklin's report

GEP-V Electron Trigger Rates vs. Energy, $\Omega = 174 \text{ msr}$

E

5

- Fun
- Ener
- Spat
- Full |



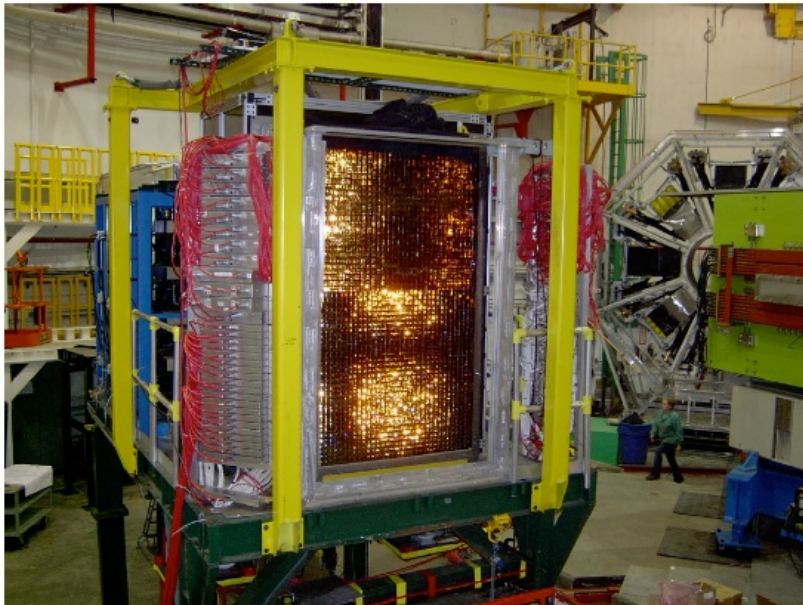
ate detector)

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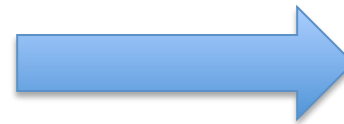
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BigCal for GEp experiment

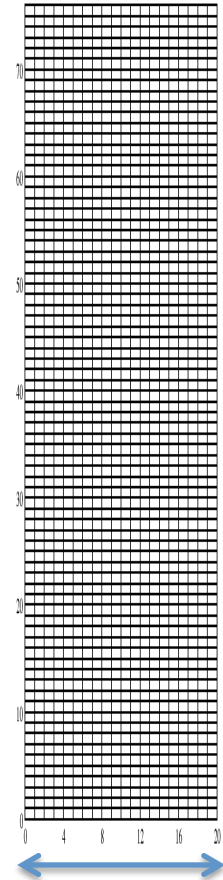
Used in Hall C GEp3



Reconfigure



76 blocks



20 blocks

- Existing **lead-glass calorimeter**
- Reconfigure: 1520 blocks ?
- Block size : $4 \times 4 \times 40 \text{ cm}^3$ and $3.8 \times 3.8 \times 45 \text{ cm}^3$
- Area: $0.80 \text{ m} \times 3.04 \text{ m} = 2.4 \text{ m}^2$

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eCal Development

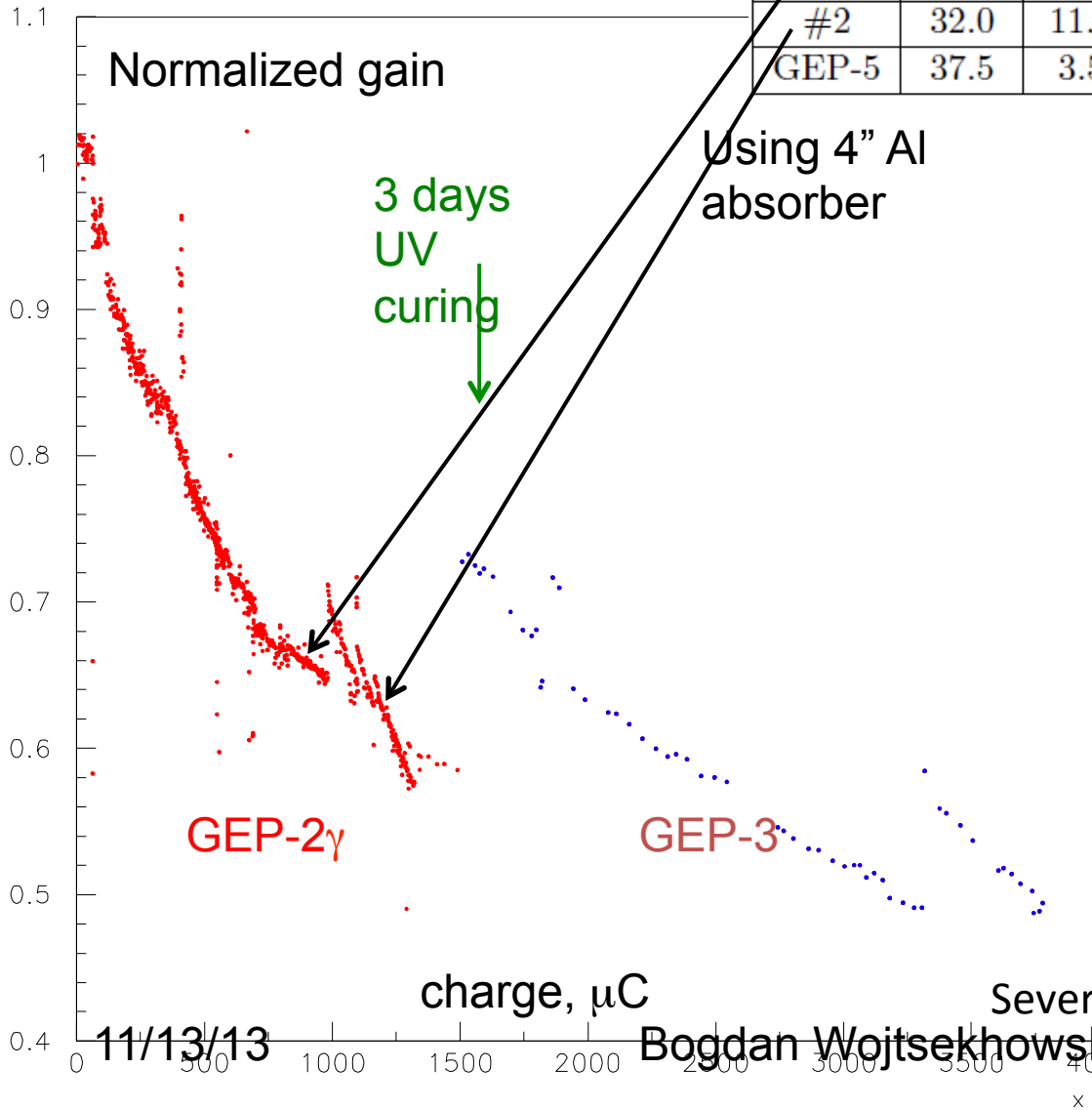
Per Review panel comment: “The lead glass radiation damage and cure rates should be tested with prototype setups under realistic conditions.”

- Plan is: UV recovery (needs 5x UV power density rel. GEp3)
 - Test irradiations at Idaho State University
 - Existing experience from GEp3
- New idea: Continual bake-out scheme
 - Heat front of crystals to 300 C, back at 250 C
 - Thermal radiation appears acceptable for PMT
 - Tests are under preparation
- Alternative to BigCal:
 - LAC calorimeter (Pb-scint. bars) from CLAS6
 - Used calorimeter from DESY

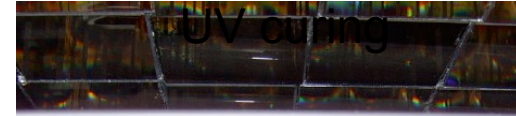
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BigCal Radiation damage and UV curing

kin.	angle deg.	Dist. m	Target cm	E GeV	Gain loss rate b	soft photon flux $J/cm^2/C$
#1	44.9	12	20	2.839	0.14%/C	0.0039
#2	32.0	11.2	20	3.539	0.53%/C	0.013
GEP-5	37.5	3.5	40	3.539	~6.7%/C	0.17



Data Geant3 simulations
estimation



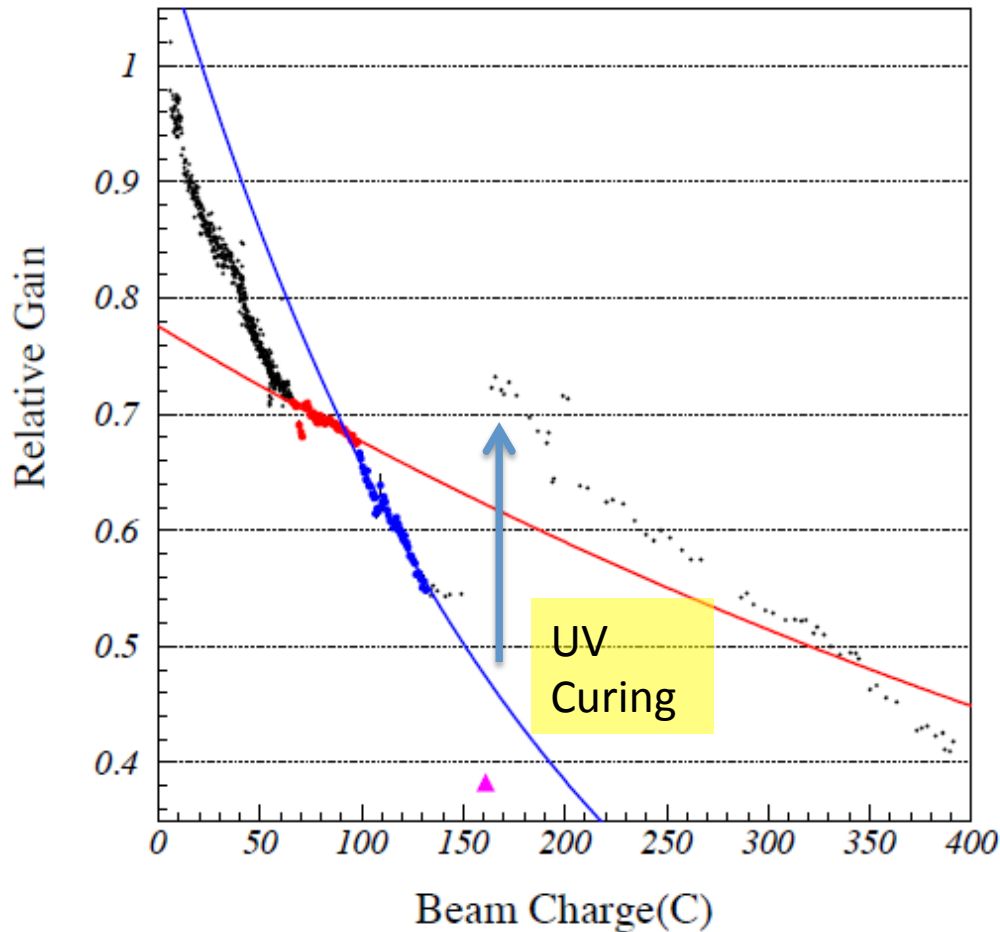
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ECAL version #1 is based on lead glass annealing

1. UV-induced annealing
2. Thermal annealing

UV Curing



Hall C Experience:

- UV cured the BigCal for 3 days on each $\frac{1}{4}$ of the detector.
- Improved the gain from 39% to 74%
- Rate of improvement is 1.24%/hr

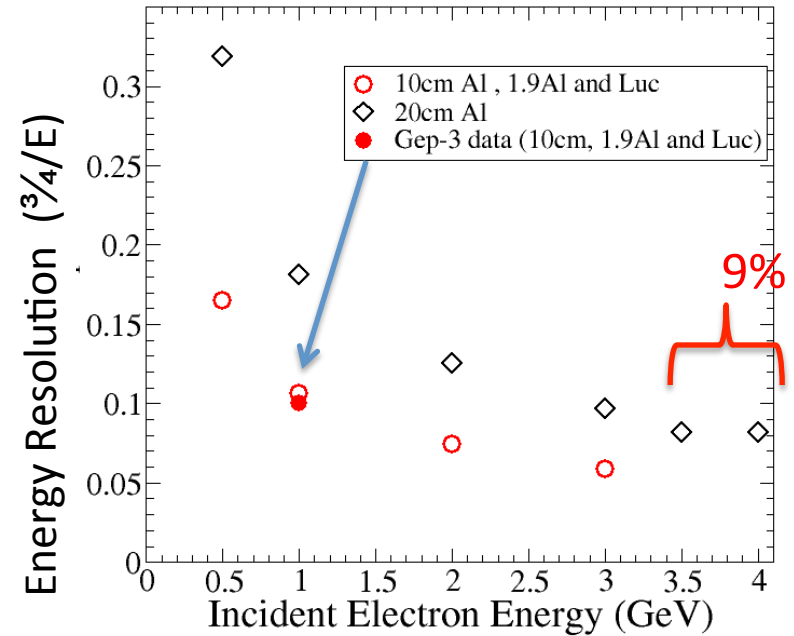
GEp5:

- Need to be cured 6% /hr
- Will increase UV intensity by x5
- UV cure for 1hr after 7 hours of running. (Need to have HV off)

BigCal Performance

Energy Resolution

Simulation shows 10% energy resolution maintained even after increasing absorber thickness

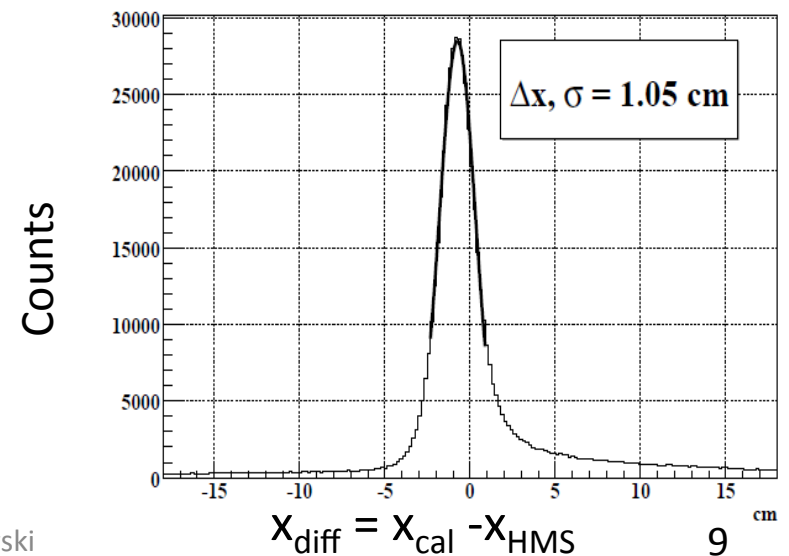


Spatial Resolution

Measured in GEp3

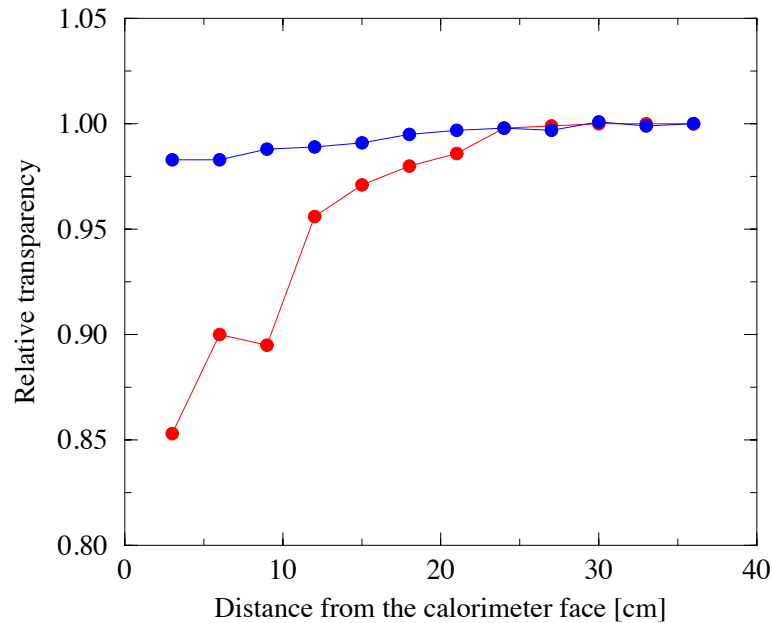
Subtract contributions of HMS,
add additional absorber

=> Achieve $\sigma \sim 6$ mm

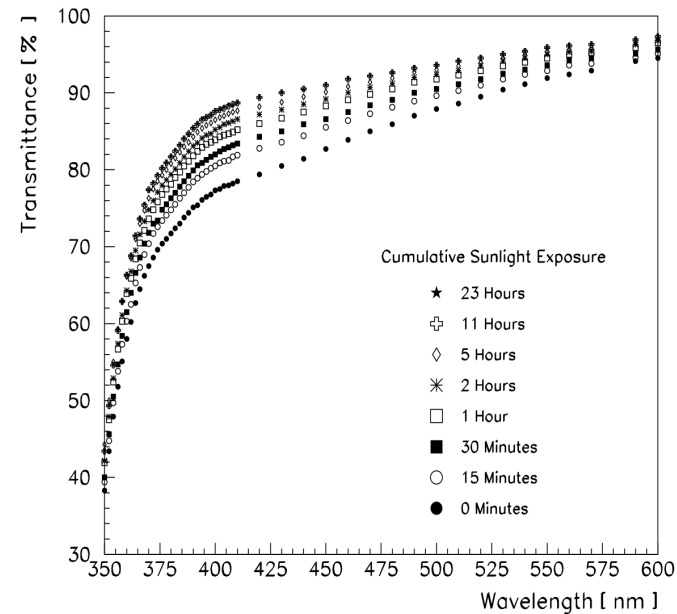


Radiation damage

RCS calorimeter study



from E790 thesis



Variation of optical band gap with radiation dose in $\text{PbO-B}_2\text{O}_3$ glasses

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Radiation damage

Radiation Damage of F8 Lead Glass with 20 MeV Electrons

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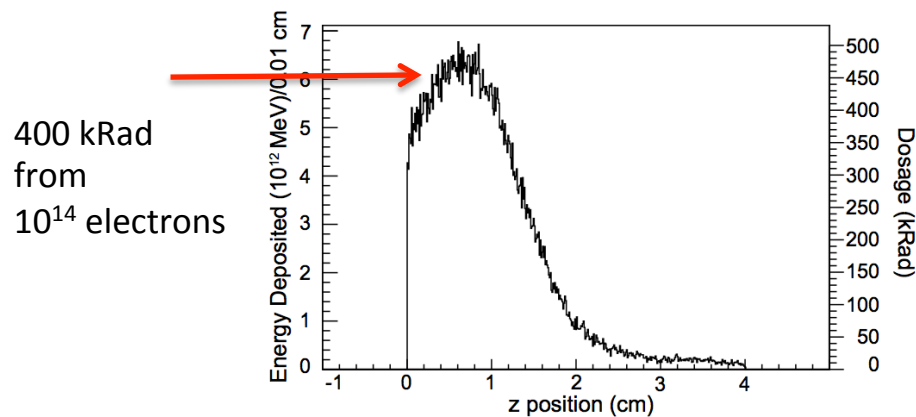


Figure 4: GEANT4 simulation of energy deposition of 10^{14} 20 MeV electrons as a function of depth in a $2.4 \text{ cm} \times 2.5 \text{ cm} \times 4 \text{ cm}$ volume of lead glass. The dosage scale assumes a volume element of $2.4 \text{ cm} \times 2.5 \text{ cm} \times 0.01 \text{ cm}$.

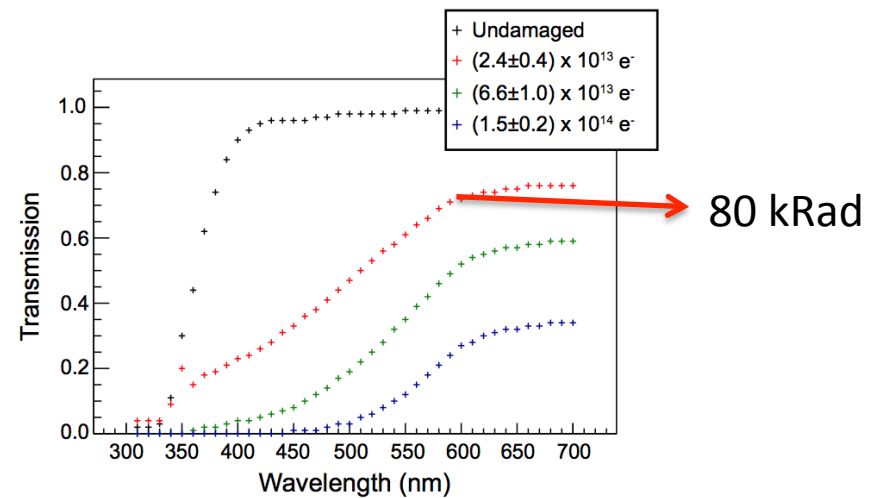


Figure 5: Transmission coefficient of 4 cm of lead glass as a function of wavelength for various amounts of radiation. Estimated errors are 2% (10%) for wavelengths above (below) 380 nm.

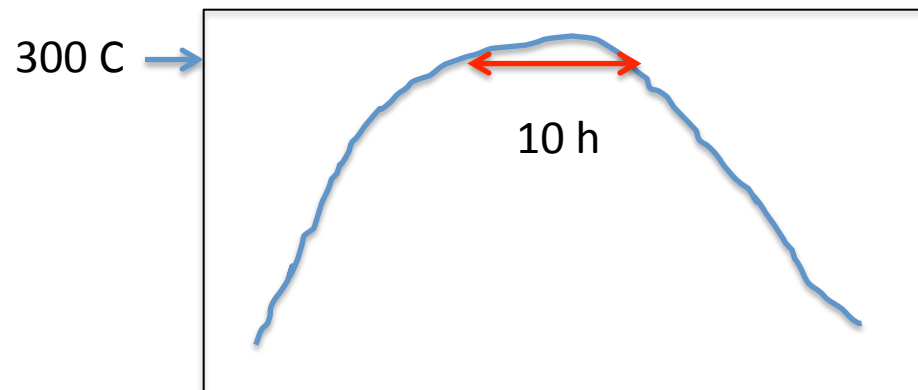
ECAL with Thermal annealing of lead glass in situ

1. Experimental data on thermal annealing
2. Annealing speed and Electrical conductivity vs. temperature
3. PMT dark current induced thermal radiation
 - a) Emissivity of glass and a heater
 - b) Test result
4. Temperature distribution and stresses
5. Power of heating
 - a) Heat conductivity of glass, glass wool
 - b) First test with front heater

ECAL with Thermal annealing of lead glass in situ

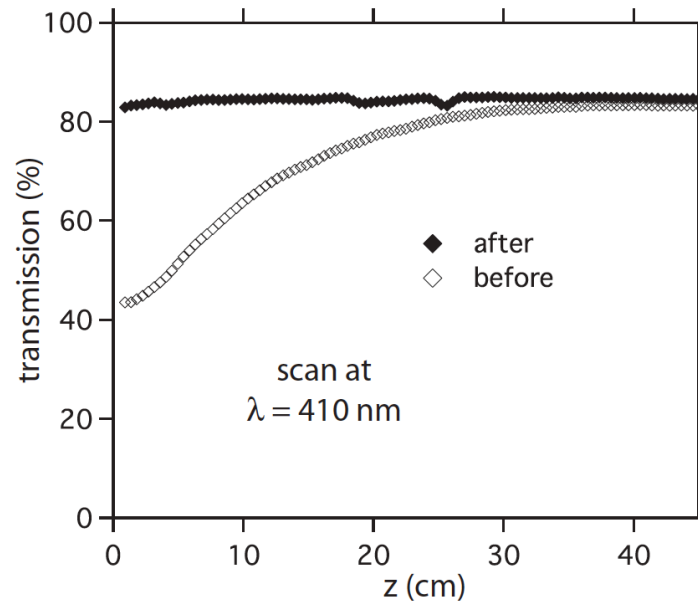
Experimental data on thermal annealing

- a) 200 HRS shower blocks
- b) Few RCS blocks
- c) 600 Hall D blocks



ECAL with Thermal annealing of lead glass in situ

Figure 4.4 shows the transmission of light, at $\lambda = 410$ nm, through 4 cm of lead glass as a function of distance along the bar for a radiation-damaged bar before and after heat curing at 260 °C. The $z = 0$ position corresponds to the upstream end of the bar during data taking, *i.e.* the end of the bar closest to the source of the photon beam.



12 hours
at 260 C
household
oven

Figure 4.4: Transmission of light, at $\lambda = 410$ nm, through 4 cm of lead glass as a function of distance along the bar for a radiation-damaged bar before and after heat curing at 260 °C.

Electrical conductivity of glass

<u>Material: Glass (SiO₂), bulk.</u> MEMS and Nanotechnology Clearinghouse.	<u>Property</u>	<u>Value</u>	<u>Conditions</u>	790 Ωm to 3.98 × 10 ¹¹ Ωm
	Electrical resistivity	1e+09 ... 3.98e+11 Ω*m	Glass,at temp=250 C	
	Electrical resistivity	3.16e+06 ... 6.3e+08 Ω*m	Glass,at temp=400 C	
	Electrical resistivity	630000 Ω*m	Glass,at temp=500 C	
	Electrical resistivity	4600 Ω*m	Glass,at temp=1000 C	
	Electrical resistivity	790 Ω*m	Glass,at temp=1500 C	

At ~400 C change by a factor of 1000 per 100 degrees

Measurement for the lead glass is needed!

Electrical conductivity of glass

$$\Omega = C \times 10^{(4500/T)}$$

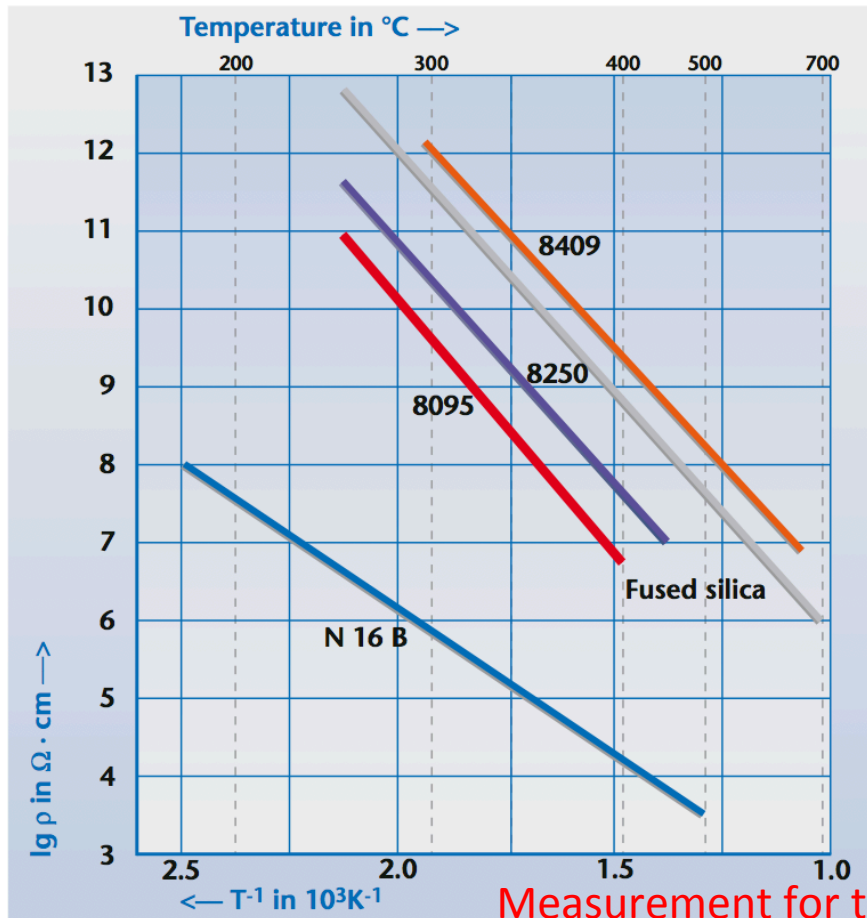


Fig. 21. Electrical volume resistivity of various technical glasses and fused silica related to the reciprocal of absolute temperature

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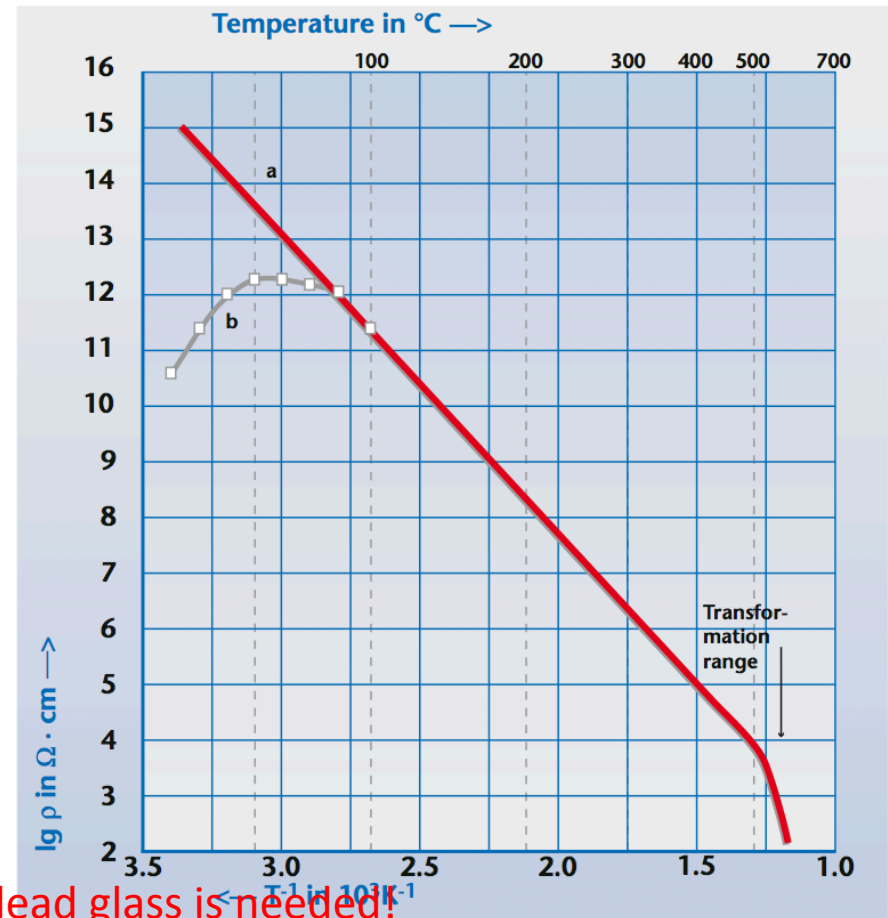


Fig. 22. Electrical resistance ρ of a soda-lime glass related to temperature (a) without, and (b) with hydrated layer

Measurement for the lead glass is needed!

PMT dark current induced TR

a) Emissivity of glass and a heater

100% = Emissivity + Transmissivity + Reflectivity

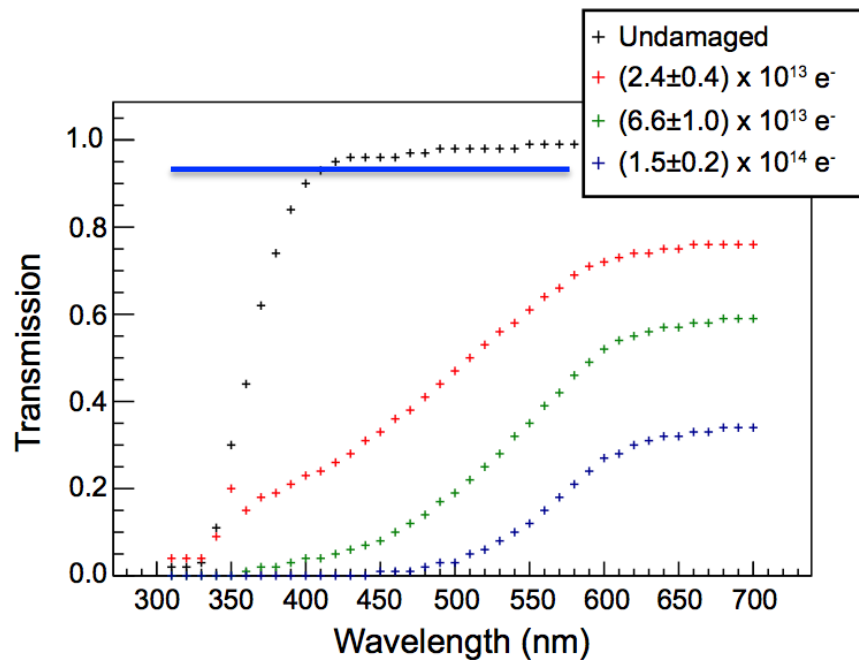


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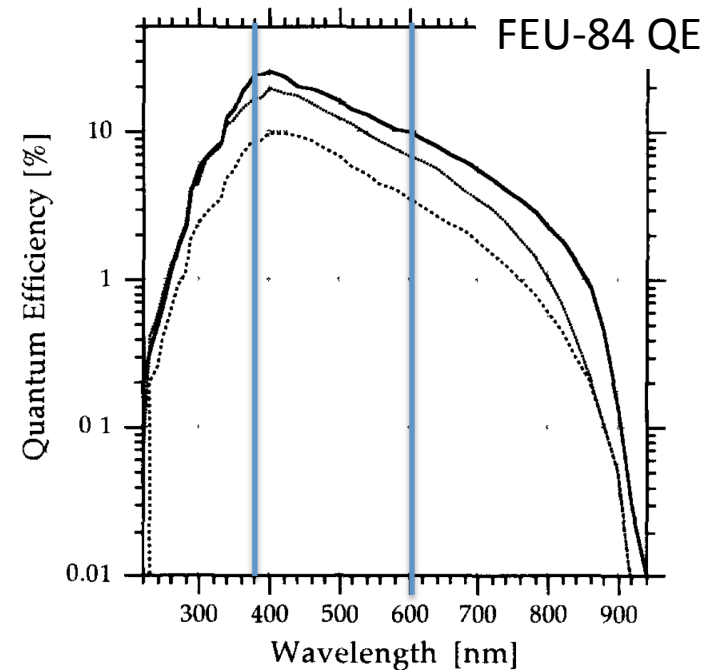


Fig. 4. The absolute quantum efficiency of three FEU-84-3 phototubes as measured by Hamamatsu Inc. using a calibrated source. Three tubes were selected, using the method described in the text, as having relatively high, medium and low relative quantum efficiencies.

PMT dark current induced TR

a) Emissivity of **glass** and a heater

$$J_{ph} \propto \exp(-h\nu/kT)$$

100% = Emissivity + Transmissivity + Reflectivity

$$kT \sim 1/20 \text{ eV}; h\nu \sim 3 \text{ eV}$$

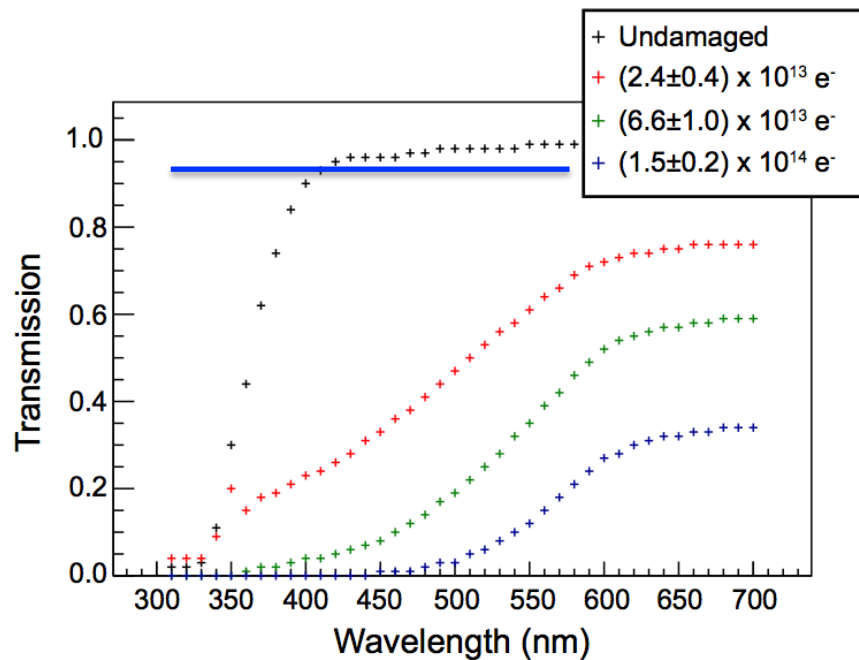


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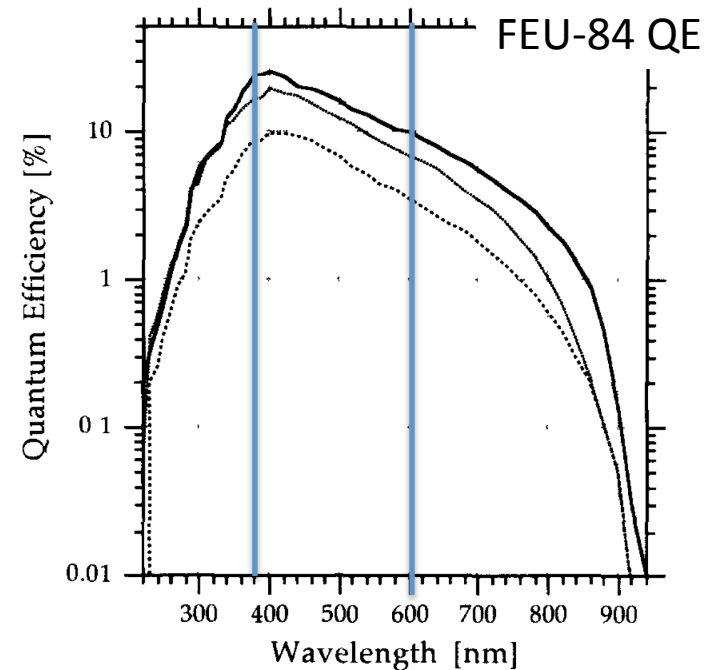


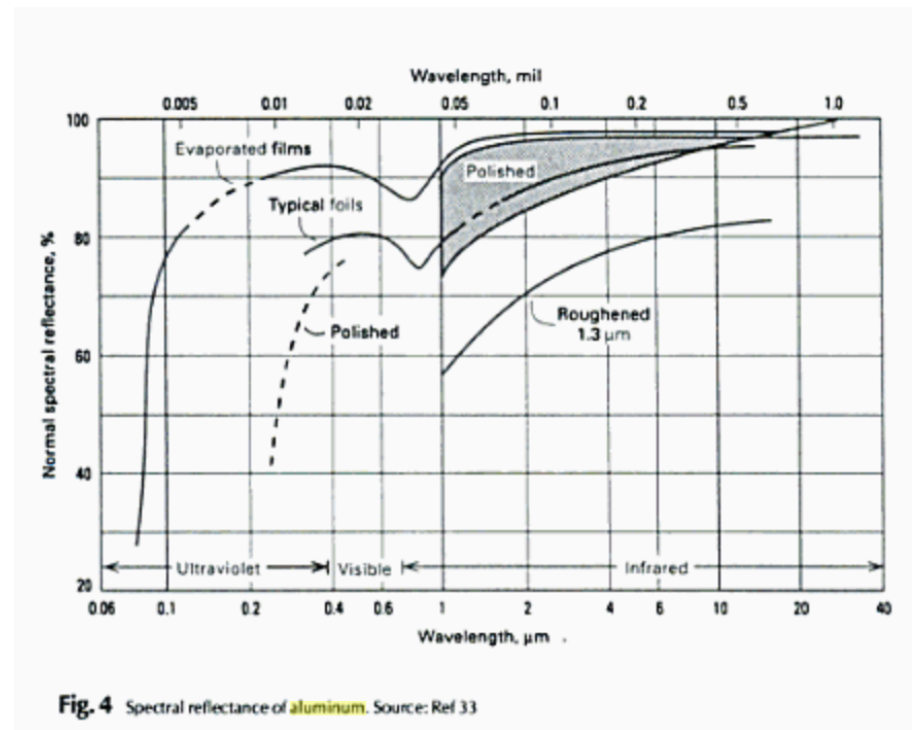
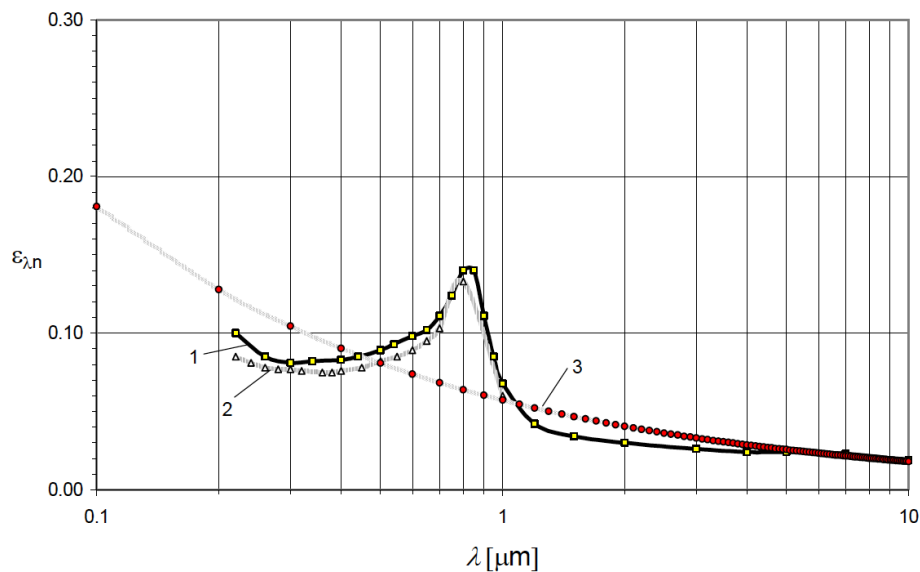
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PMT dark current induced TR

a) Emissivity of glass and a heater

100% = Emissivity + Transmissivity + Reflectivity

A polished aluminum surface with emissivity = 0.12 has reflectivity = 0.88.



PMT dark current induced TR

a) Emissivity of glass and a heater

- Mechanics
- Miscellaneous
- Physiology
- Piping Systems
- Process Control
- Pumps
- Standards Organizations
- Steam and Condensate
- Thermodynamics
- Water Systems

AdChoices 

- [▶ Copper Wire](#)
- [▶ Carbon Steel](#)
- [▶ Sheet Steel](#)

[Convert Units](#)

[Temperature](#)

 °C

 °F

[Length](#)

Surface Material	Emissivity Coefficient - ε -
Alloy 24ST Polished	0.09
Alumina, Flame sprayed	0.8
Aluminum Commercial sheet	0.09
Aluminum Foil	0.04
Aluminum Commercial Sheet	0.09
Aluminum Heavily Oxidized	0.2 - 0.31
Aluminum Highly Polished	0.039 - 0.057
Aluminum Anodized	0.77
Aluminum Rough	0.07
Aluminum paint	0.27 - 0.67
Antimony, polished	0.28 - 0.31
Asbestos board	0.96
Asbestos paper	0.93 - 0.945
Asphalt	0.93
Basalt	0.72
Beryllium	0.18
Beryllium, Anodized	0.9
Bismuth, bright	0.34
Black Body Matt	1.00
Black lacquer on iron	0.875



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PMT dark current induced TR



- a) Emissivity of glass and a heater
- b) **Test result**



With 300 C on Al (not polished) heater the anode current was measured in the PMT attached to the lead glass module (at room T). Projected to the actual gain in GEp5 experiment the current is of **170 nA**. Such a current will shift the pedestal by 1.7 MeV. Further reduction by a factor of 5 is due to low emissivity of polished Al

heater



FEU-84-3

Thermal stress

Example 2.8 When a beam of a rectangular cross section $b \times h$ is subjected to a temperature change $T(y, z) = C_0 + C_1y + C_2z$, what thermal stress is produced in the beam?

Solution The substitution of the temperature change $T(y, z) = C_0 + C_1y + C_2z$ into equation 2.5.1 gives



$$\int_A \alpha E T(y, z) dA$$

$$\int_{-b/2}^{b/2} \int_{-h/2}^{h/2} \alpha E (C_0 + C_1y + C_2z) dy dz = \alpha E b h C_0$$

$$\int_A \alpha E T(y, z) z dA$$

$$\int_{-b/2}^{b/2} \int_{-h/2}^{h/2} \alpha E (C_0z + C_1yz + C_2z^2) dy dz = \frac{1}{12} \alpha E b^3 h C_2$$

$$\int_A \alpha E T(y, z) y dA$$

$$\int_{-b/2}^{b/2} \int_{-h/2}^{h/2} \alpha E (C_0y + C_1y^2 + C_2yz) dy dz = \frac{1}{12} \alpha E b h^3 C_1$$

$$A = bh, \quad I_z = \frac{1}{12} b h^3, \quad I_y = \frac{1}{12} b^3 h, \quad I_{yz} = 0$$

Thermal stress (2.37) reduces to

$$\sigma_x = -\alpha E (C_0 + C_1y + C_2z) + \frac{\alpha E b h C_0}{b h} + \frac{\alpha E b h^3 C_1 / 12}{b h^3 / 12} y + \frac{\alpha E b^3 h C_2 / 12}{b^3 h / 12} z = 0$$

Longitudinal gradient

Heat leak to the sides is the only concern: It creates the stress

250	250
	300
250	250

The parameters of glass

Main properties of soda lime silicate glass

Volumic mass ρ at 18°C	2,500 kg/m ³
Young's modulus (E)	70,000 N/mm ²
Modulus of rigidity (G)	29,166 N/mm ²
Poisson's ratio (ν)	0.2
Mohs' hardness	6
Melting temperature	≈ 1,500°C
Softening point	≈ 600°C
Linear expansion coefficient (α)	9.10 ⁻⁶ m/(m.K)
Thermal conductivity (λ)	1 W/(m.K)
Specific heat capacity (c)	720 J/(kg.K)
Characteristic bending strength:	
annealed glass *	45 N/mm ²
heat-strengthened glass *	70 N/mm ²
thermally toughened glass *	120 N/mm ²
Compression resistance	1000 N/mm ²
Thermal transmittance (single glazing 4 mm)	5.8 W/(m ² .K)
Refraction index (n) compared to air	1.5
Light transmission (single glazing 4 mm)	0.90
Solar factor (single glazing 4 mm)	0.87
Normal emissivity of non-coated glass or coated glass with no impact on emissivity	0.89

Acceptable temperature "gradient" is of 50 C/cm

Heating power in situ

Thermal Conductivity - k - (W/m.K)			
Material	Temperature (°C)		
	25	125	225
Acetone	0.16		
Acrylic	0.2		
Air	0.024		
Aluminum	250	255	250
Ammonia	0.022		
Antimony	18.5		
Argon	0.016		
Asphalt	1.26		
Balsa	0.048		
Bitumen	0.17		
Benzene	0.16		
Beryllium	218		
Brass	109		
Brick dense	1.6		
Brick work	0.5		
Cadmium	92		
Carbon	1.7		
Cement	1.01		
Cobalt	69		
Concrete	1.05		
Constantan	22		
Copper	401	400	398
Carbon Steel	54	51	47
Cotton Wool insulation	0.029		
Ether	0.14		
Epoxy	0.35		
Felt insulation	0.04		
Glass	1.05		
Glass Wool insulation	0.04		
Glycerol	0.28		
Gold	310	312	310

a) Heat conductivity of glass, glass wool

b) First test with front heater: 30 C/cm

For 40-cm long block at $T_1=300$ C and $T_2=50$ C

the power is 1 Watt/block => total for system of 2000 blocks is of **2 kW**

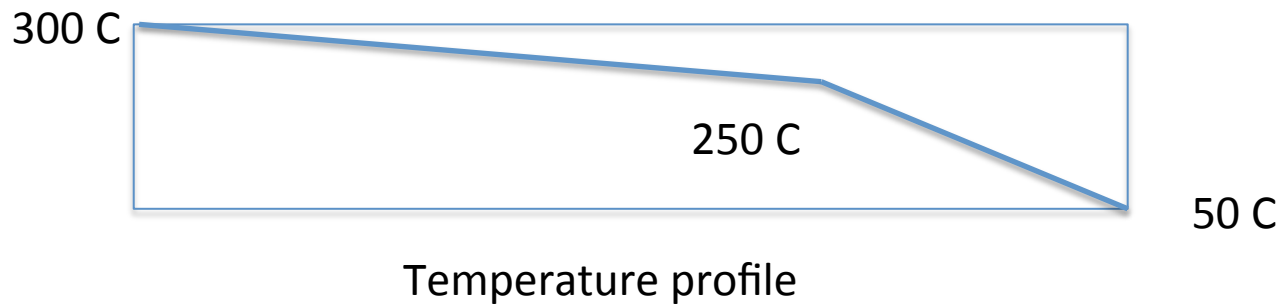
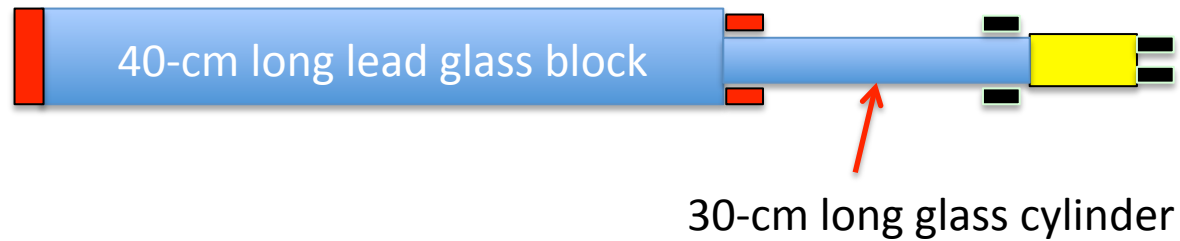
Glass wool layer around: $t = 27$ cm, area ~ 10 m² => **0.4 kW**

Maybe need to add a distributed heater on the periphery of the calorimeter

1.05 Watt/m/C

0.04 Watt/m/C

The scheme under investigation



$$0.008 \times 7 \times 200 / 30 = 0.4 \text{ W heat through light guide}$$

The items to do for ECAL

1. Inventory of the available equipment

- i) Lead glass blocks
- ii) PMTs
- iii) HV bases
- iv) Front-end electronics
- v) Cables (signal and HV)
- vi) HV supplies
- vii) NIM electronics

2. Investigation of the Thermal annealing

- i) Measure DC for full proposed configuration
- ii) Design of 5x5 module
- iii) Irradiate 10 blocks and test TA in oven
- iv) Measure electrical conductivity vs. T
- v) Develop the budget of the 5x5 module
- vi) Construct 5x5 module
- vii) Full test at Idaho State University

3. Preparation of the required equipment

- i) PMTs – test gain, QE
- ii) HV bases – test, repair
- iii)